

## High Efficiency, 15A Synchronous Step Up Regulator with Accurate Output Current Limit

### General Description

The SY21225 is a high efficiency synchronous boost regulator with programmable output current limit. The device uses adaptive constant off time and current mode control. The integrated low  $R_{DS(ON)}$  switches minimize the conduction loss.

The SY21225 features cycle-by-cycle peak current limit, output short circuit protection and true shutdown. The device also provides enable control and a power good indicator which can be used for system power sequencing. Low output voltage ripple and small external inductor and capacitor sizes can be achieved with a resistor programmable pseudo-constant frequency.

The SY21225 is available in a 4 mm x 4mm QFN package.

### Features

- Input Voltage Range: 4.5-30V
- Programmable Pseudo-Constant Frequency 200kHz to 1MHz
- Low  $R_{DS(ON)}$  Internal Switches  
Main FET: 16m $\Omega$   
Rectifier FET: 18m $\Omega$   
Disconnect FET: 18m $\Omega$
- True Shutdown Function
- Programmable Output Current Limit
- Internal Soft-start Limits the Inrush Current
- Input Voltage UVLO
- Over Temperature Protection
- Over Voltage Protection
- Output Short Circuit Protection
- Minimum ON Time: 100ns typical
- Minimum OFF Time: 120ns typical

### Applications

- Power Bank
- High Power AP

### Typical Applications

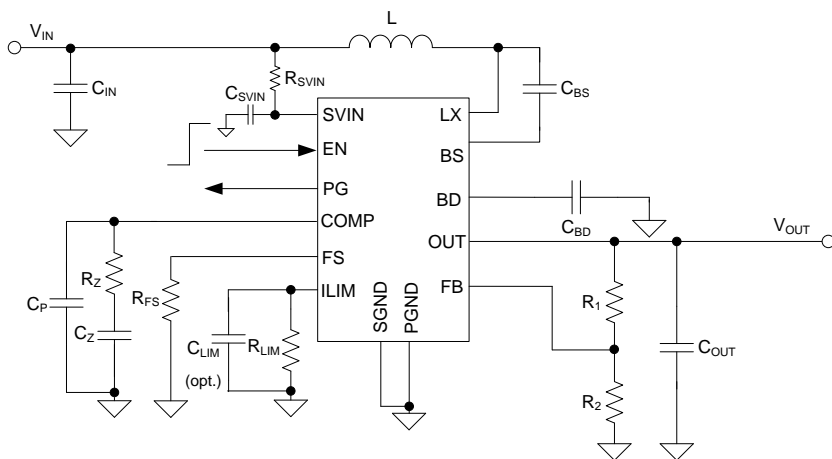


Figure1. Schematic Diagram

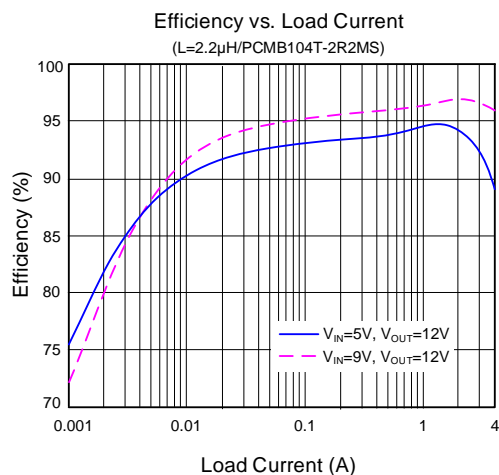


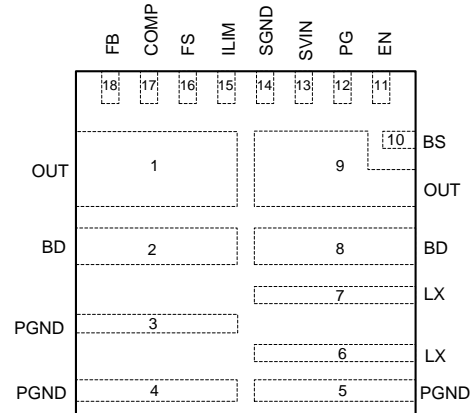
Figure2. Efficiency vs. Load Current

## Ordering Information

Ordering Part Number	Package Type	Top Mark
SY21225RDC	QFN4x4-18 RoHS Compliant and Halogen Free	AVZxyz

*x=year code, y=week code, z=lot number code*

## Pinout (top view)



## Pin Description

Pin Name	Pin Number	Pin Description
OUT	1,9	The Boost converter output pin.
BD	2,8	Connect to the Drain of internal Disconnect FET. Bypass at least a 4.7μF ceramic capacitor to PGND.
PGND	3,4,5	Power ground pin.
LX	6,7	Inductor node. Connect an inductor from power input to the LX pin.
BS	10	Boot-strap pin. Supply Rectified FET's gate driver. Connect a 0.1μF ceramic capacitor between the BS pin and the LX pin.
EN	11	Enable control. Pull high to turn on the IC. Do not leave it floating.
PG	12	Power good indicator. Open drain output, driven low when the output < 90% of the target regulation voltage, high impedance otherwise.
SVIN	13	Device power supply pin. Decouple this pin to the SGND pin with a 2.2μF ceramic capacitor.
SGND	14	Signal ground pin.
ILIM	15	Output current limit program pin. Connect a resistor $R_{LIM}$ from this pin to SGND to program output current limitation threshold. $I_{LIM}(A) = 30(V) / R_{LIM}(k\Omega)$
FS	16	Switching frequency configuration pin. Connect a resistor from this pin to ground to program the switching frequency. $f_{SW}(kHz) = 1.4 \times 10^6 / R_{FS}(\Omega)^{0.645}$ .
COMP	17	Loop compensation pin. Connect a RC network across this pin and ground to stabilize the control loop.
FB	18	Feedback pin. Connect to the center of resistor voltage divider to program the output voltage: $V_{OUT} = 1V \times (R_1 / R_2 + 1)$

## Block Diagram

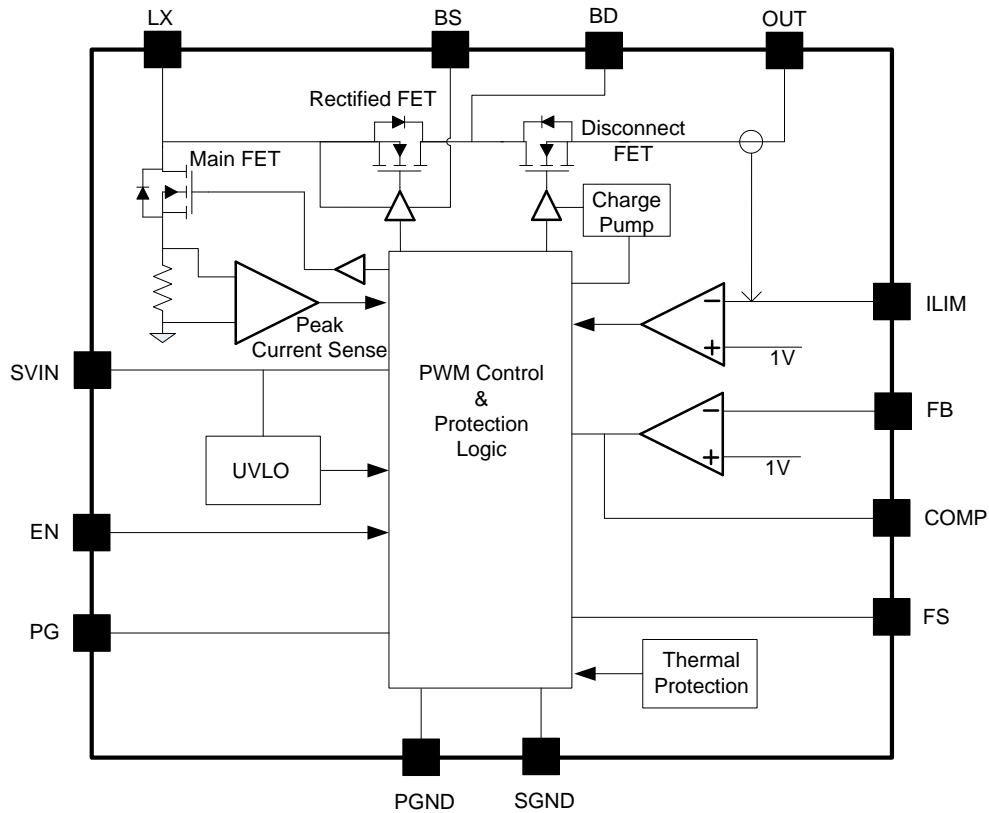


Figure3. Block Diagram

## Absolute Maximum Ratings

Parameter (Note1)	Min	Max	Unit
SVIN, LX, EN, ILIM, OUT, BD, FS, PG, COMP	-0.3	33	V
FB, BS-LX	-0.3	4	
LX, 10ns Duration	-3.5	36	
Lead Temperature (Soldering, 10 sec.)		260	°C
Junction Temperature, Operating	-40	150	
Storage Temperature	-65	150	

## Thermal Information

Parameter (Note2)	Typ	Unit
$\theta_{JA}$ Junction-to-ambient Thermal Resistance	30	°C/W
$\theta_{JC}$ Junction-to-case Thermal Resistance	3.2	
$P_D$ Power Dissipation $T_A=25^\circ\text{C}$	3.4	W

## Recommended Operating Conditions

Parameter (Note3)	Min	Max	Unit
SVIN	4.5	30	V
Junction Temperature, Operating	-40	125	°C
Ambient Temperature	-40	85	

## Electrical Characteristics

( $V_{IN}=5V$ ,  $V_{OUT}=12V$ ,  $I_{OUT}=100mA$ ,  $T_A=25^{\circ}C$ , unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Input Voltage Range	$V_{IN}$		4.5		30	V
Input UVLO Threshold	$V_{UVLO}$			4	4.35	V
UVLO Hysteresis	$V_{HYS}$			0.2		V
Quiescent Current	$I_Q$	$V_{OUT}=13V$			230	$\mu A$
Shutdown Current	$I_{SHDN}$	$EN=0$			5	$\mu A$
Feedback Reference Voltage	$V_{REF}$		0.985	1	1.015	V
FB Input Current	$I_{FB}$	$V_{FB}=2V$	-50		50	nA
Main FET RON	$R_{DS(ON),M}$			16		m $\Omega$
Rectifier FET RON	$R_{DS(ON),R}$			18		m $\Omega$
Disconnect FET RON	$R_{DS(ON),D}$			18		m $\Omega$
EN Rising Threshold	$V_{ENH}$		1.5			V
EN Falling Threshold	$V_{ENL}$				0.4	V
Min ON Time	$t_{ON,MIN}$			100		ns
Min OFF Time	$t_{OFF,MIN}$			120		ns
Switching Frequency	$f_{SW}$	$R_{FS}=390k\Omega$		345		kHz
Switching Frequency Programmable Range			200		1000	kHz
Power Good Threshold	$V_{PG}$	$V_{FB}$ Rising (Good)		90		% $V_{REF}$
Power Good Hysteresis	$V_{PG,HYS}$			2.5		% $V_{REF}$
Power Good Delay	$t_{PG,RISING}$	Low to high		40		$\mu s$
	$t_{PG,FALLING}$	High to low		30		$\mu s$
Power Good Output Low	$V_{PGL}$	$I_{PG}=4mA$		0.15		V
BD Over Voltage Threshold	$V_{OVP}$	$V_{FB}$ Rising	31			V
BD Over Voltage Hysteresis	$V_{OVP,HYS}$			0.5		V
BD OVP Delay	$t_{OVP,DLY}$			5		$\mu s$
Output Under Voltage Protection Threshold	$V_{UVP}$			2		V
Output UVP Delay	$t_{UVP,DLY}$			2		$\mu s$
Hic-cup ON Time	$t_{UVP,ON}$			2		ms
Hic-cup OFF Time	$t_{UVP,OFF}$			12		ms
Main N-FET Current Limit	$I_{LIM,PEAK}$		15		21	A
Output Current Limit Programmable Range	$I_{LIM,OUT}$		1		4	A
Output Current Limit Accuracy	$I_{LMT,ACC}$		-25		25	%
Output Current Limit Reference Voltage	$V_{LIM}$			1		V
Error Amplifier Trans-conductance	$g_m$			100		$\mu S$
Current Sense Gain	$R_i$			75		m $\Omega$
Thermal Shutdown Temperature	$T_{SD}$			150		$^{\circ}C$
Thermal Shutdown Hysteresis	$T_{HYS}$			15		$^{\circ}C$



# SY21225

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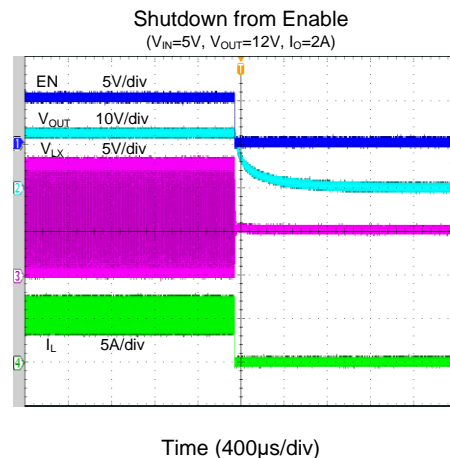
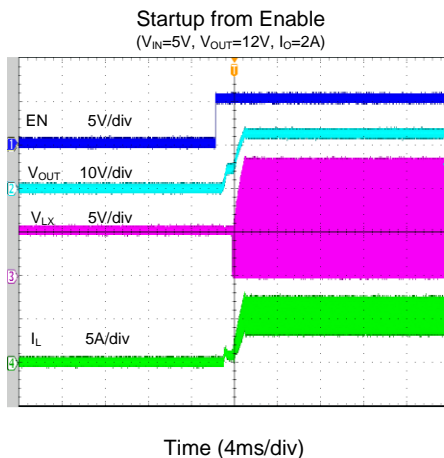
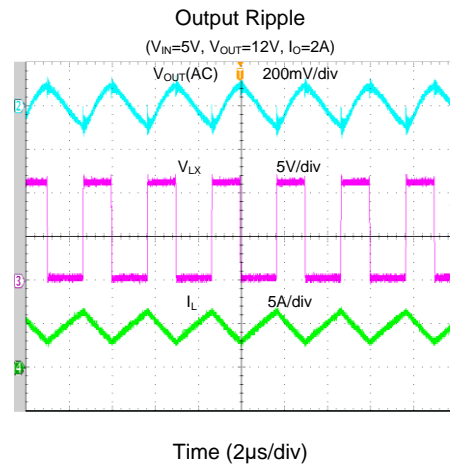
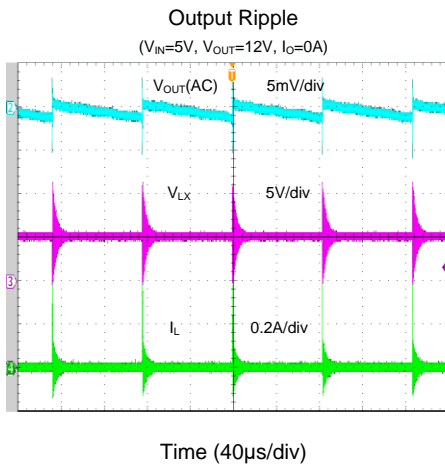
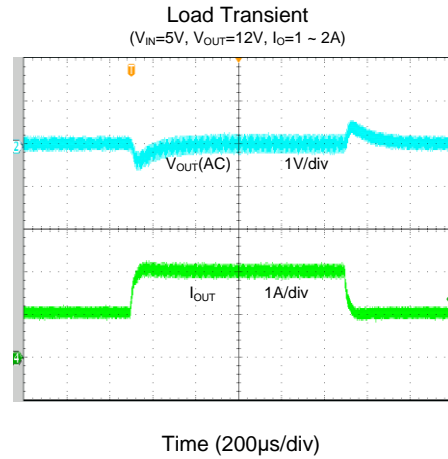
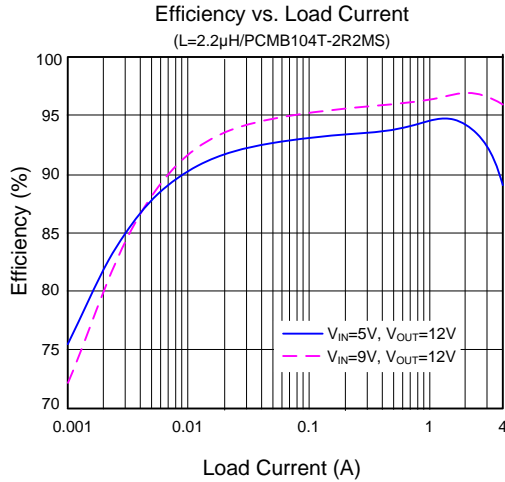
**Note 1:** Stresses beyond the “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specification is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

**Note 2:**  $\theta_{JA}$  is measured in the natural convection at  $T_A = 25^\circ\text{C}$  on a two-layer Silergy Evaluation Board.

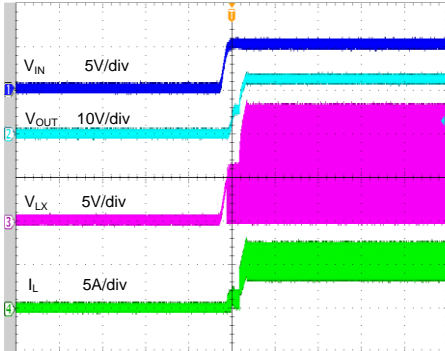
**Note 3:** The device is not guaranteed to function outside its operating conditions.

## Typical Performance Characteristics

( $T_A = 25^\circ\text{C}$ ,  $V_{OUT} = 12\text{V}$ ,  $f_{SW} = 350\text{kHz}$ ,  $L = 2.2\mu\text{H}$ ,  $C_{OUT} = 44\mu\text{F}$ , unless otherwise specified.)

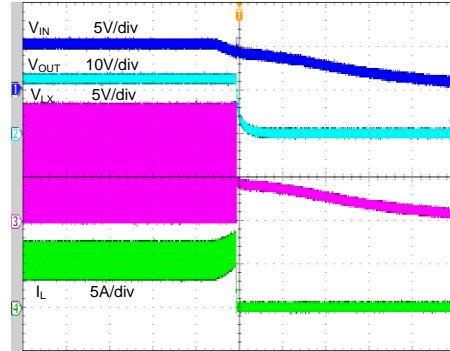


Startup from  $V_{IN}$   
( $V_{IN}=5V$ ,  $V_{OUT}=12V$ ,  $I_O=2A$ )



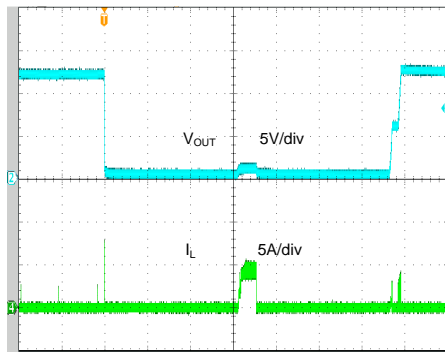
Time (4ms/div)

Shutdown from  $V_{IN}$   
( $V_{IN}=5V$ ,  $V_{OUT}=12V$ ,  $I_O=2A$ )



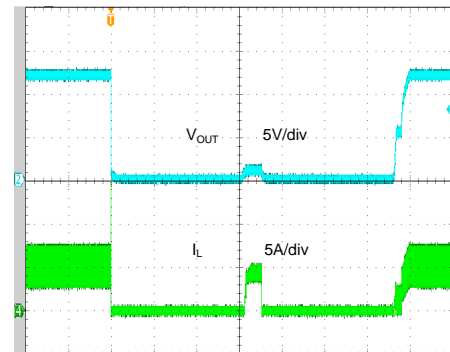
Time (2ms/div)

Short Circuit Protection  
( $V_{IN}=5V$ ,  $V_{OUT}=12V$ ,  $I_O=0A$  ~ short)



Time (4ms/div)

Short Circuit Protection  
( $V_{IN}=5V$ ,  $V_{OUT}=12V$ ,  $I_O=2A$  ~ short)



Time (4ms/div)

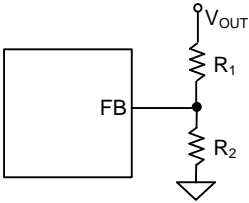
## Applications Information

The following paragraphs provide information on the selection of the input capacitor  $C_{IN}$ , the output capacitor  $C_{OUT}$ , the output current limiting resistor  $R_{LIM}$ , the switching frequency programming resistor  $R_{FS}$ , the inductor  $L$  and the feedback resistors ( $R_1$  and  $R_2$ ).

### Feedback Resistor divider $R_1$ and $R_2$

Choose  $R_1$  and  $R_2$  to program the proper output voltage. To minimize the power consumption under light load, it is desirable to choose large resistance values for both  $R_1$  and  $R_2$ . A value between 10k and 1M is recommended for both resistors. If  $R_1=200k$  is chosen, then  $R_2$  can be calculated to be:

$$R_2 = \frac{R_1}{V_{OUT} - 1} (\Omega)$$



### Input Capacitor $C_{IN}$

The ripple current through input capacitor is calculated as:

$$I_{CIN\_RMS} = \frac{V_{IN} \times (V_{OUT} - V_{IN})}{2\sqrt{3} \times L \times f_{sw} \times V_{OUT}} (A)$$

To minimize the system switching noise, place a typical X5R or better grade ceramic capacitor close to the inductor and PGND pin. Care should be taken to minimize the loop area formed by  $C_{IN}$ ,  $V_{IN}$ , and the PGND pins. A 10 $\mu$ F low ESR ceramic capacitor is recommended for most applications.

### Input Capacitor $C_{SVIN}$

The  $SVIN$  capacitor must be placed close to the  $SVIN$  and  $SGND$  pins. Care should be taken to minimize the loop area formed by the capacitor and the  $SVIN/SGND$  pins. A 2.2 $\mu$ F low ESR ceramic capacitor is recommended for most applications.

Adding the resistor  $R_{SVIN}$  with a value of 10  $\Omega$  between the  $V_{IN}$  pin and the device power input  $SVIN$  is recommended.

### Boost Output Capacitor $C_{BD}$ and Disconnection FET Output Capacitor $C_{OUT}$

The Boost Output capacitor  $C_{BD}$  and disconnection FET Output capacitor  $C_{OUT}$  are selected to handle the output ripple noise requirements. Both steady state ripple and

transient requirements must be taken into account when selecting these capacitors. For the best performance, it is recommended to use a X5R or better grade ceramic capacitors with 25V rating and more than 22 $\mu$ F capacitance.

### Boost Inductor $L$

There are several considerations in choosing this inductor.

- 1) Choose the inductance to provide the desired ripple current. It is suggested to choose the ripple current to be about 40% of the maximum average input current. The inductance is calculated as:

$$L = \left( \frac{V_{IN}}{V_{OUT}} \right)^2 \frac{(V_{OUT} - V_{IN})}{f_{sw} \times I_{OUT\_MAX} \times 40\%} (H)$$

Where  $f_{sw}$  is the switching frequency and  $I_{OUT\_MAX}$  is the maximum load current.

The SY21225 regulator is less sensitive to the ripple current variations. Consequently, the final choice of inductance can be slightly different than the calculated value without significantly impacting the performance.

- 2) The saturation current rating of an inductor must be selected to guarantee an adequate margin to the peak inductor current under full load conditions.

$$I_{SAT\_MIN} > \left( \frac{V_{OUT}}{V_{IN}} \right) \times I_{OUT\_MAX} + \frac{V_{IN}(V_{OUT} - V_{IN})}{2 \times f_{sw} \times L \times V_{OUT}}$$

- 3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency requirements. It is desirable to choose an inductor with  $DCR < 10m\Omega$  to achieve a good overall efficiency.

### Switching Frequency

The switching frequency of the SY21225 in CCM can be programmed by adjusting the external resistor  $R_{FS}$  connected to FS pin:

$$f_{sw}(kHz) = 1.4 \times 10^6 / R_{FS}(\Omega)^{0.645}$$

Under light load conditions, the SY21225 linearly reduces the switching frequency to maintain overall high efficiency.

### Enable Operation

Pulling the EN pin low (<0.4V) disables the device operation. Driving the EN pin high (>1.5V) turns on the device, and a soft start cycle is initiated.

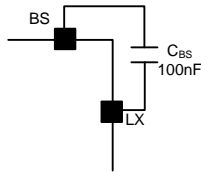


### Power Good Indication

PG is an open-drain output pin. The output is driven low if the output voltage is lower than 90% of the regulation target. Otherwise this pin will go into high impedance state.

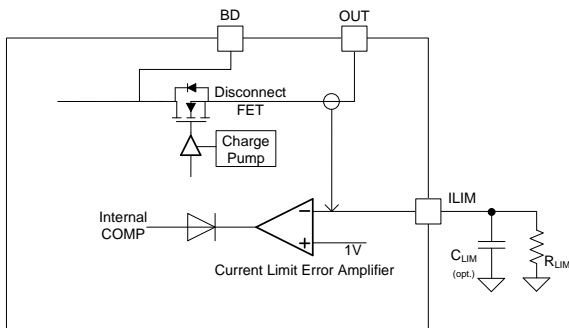
### External Bootstrap Capacitor

This capacitor provides the gate driver voltage for the internal rectifier switch. A 100nF low ESR ceramic capacitor connected between the BS and the LX pins is recommended.



### Output Current Limit

The SY21225 senses the Disconnect FET current which is fed to the ILIM pin. Simultaneously, a resistor on ILIM converts this current signal to a voltage signal that is fed to the negative input of the current-limit error amplifier. The current-limit amplifier output clamps VCOMP if the output current signal is higher than the current limit threshold. As a result, the output current is limited by the internal COMP signal, and the output voltage decreases.



$C_{LIM}$  is used for current limit signal filtering. A 10pF ceramic capacitor is recommended.  $R_{LIM}$  is used for output current limit setting. The output current limit can be programmed using the following equation:  
 $I_{LIM}(A) = 30(V) / R_{LIM}(k\Omega)$ .

### Short-circuit Protection

The SY21225 integrates a hic-cup mode short circuit protection function. If the device is operated in current limit continuously and  $V_{OUT}$  drops below 2V, the short-circuit protection mode will be initiated. The device will shut down for approximately 12ms, and then restart with a complete soft-start cycle that is approximately 2ms. The device operates in this state until the short condition disappears.

### Main FET Current Limit

The SY21225 provides a fixed cycle-by-cycle switching peak current limit. During each cycle, the internal current sensing circuit monitors the Main FET current. When the sensed current reaches the 15A (typ.) current limit, the Main FET turns off.

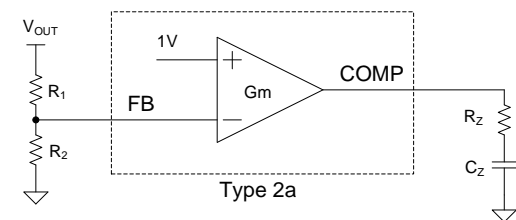
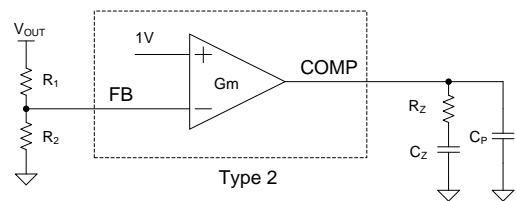
### Over-temperature Protection (OTP)

The SY21225 includes over-temperature protection (OTP) circuitry to prevent overheating due to excessive power dissipation. This will shut down switching operation when the junction temperature exceeds 150°C. Once the junction temperature cools down by approximately 15°C the IC will resume normal operation after a complete soft-start cycle. For continuous operation, provide adequate cooling so that the junction temperature does not exceed the OTP threshold.

### Loop Compensation

The SY21225 incorporates constant off time current mode control scheme. The current mode control scheme has two feedback loops. The inner current loop does not require any external compensation component. The outer voltage loop is compensated using external components.

In most applications, a Type 2 or Type 2a compensation networks shown below can be used to stabilize the voltage loop. The Type 2 is the most widely used and is recommended for power stages lagging down to -90° and where the voltage increase caused by the output capacitor ESR must be canceled. Type 2a is used in cases where the output capacitor ESR effect can be neglected.



The steps below can be used to calculate the value of external components for voltage loop compensation.

1. Select the crossover frequency  $f_c$  of the closed loop. It is recommended that the crossover frequency is chosen to be the minimum value of 1/5 of right half plane zero

( $f_{RHPZ}$ ) and 1/10 of switching frequency for a tradeoff between stability and transient response of the system. The system has faster response at higher crossover frequencies.

$$f_{RHPZ} = \frac{(1-D_{MAX})^2 \times V_{OUT}}{2\pi \times L \times I_{OUT}}$$

2. Select a  $R_Z$  value of the R-C series combination connected to the COMP pin.

$$R_Z = \frac{V_{OUT}}{g_m \times G_{fc} \times V_{REF}}$$

Where  $g_m$  is the error amplifier trans-conductance, which is typically 100uS;  $G_{fc}$  is gain of the power stage at crossover frequency.

$$G_{fc} = \frac{(1-D_{MAX})}{2\pi \times f_c \times C_{OUT} \times R_i}$$

Where  $R_i$  is the current sense gain, which is typically 75mΩ.

3. Select a  $C_Z$  value of the R-C series combination connected to the COMP pin. The compensation zero decides phase margin at the crossover frequency. Place

a compensation zero at or before the dominant pole of  $R_L$  and  $C_O$ .  $R_L$  is the load resistance, which equals to  $V_{OUT}/I_{OUT}$ .

$$C_Z = \frac{V_{OUT} \times C_{OUT}}{I_{OUT} \times R_Z}$$

4. A high frequency pole is recommended to attenuate the high frequency noise. Place this pole to cancel the ESR zero of  $C_{OUT}$

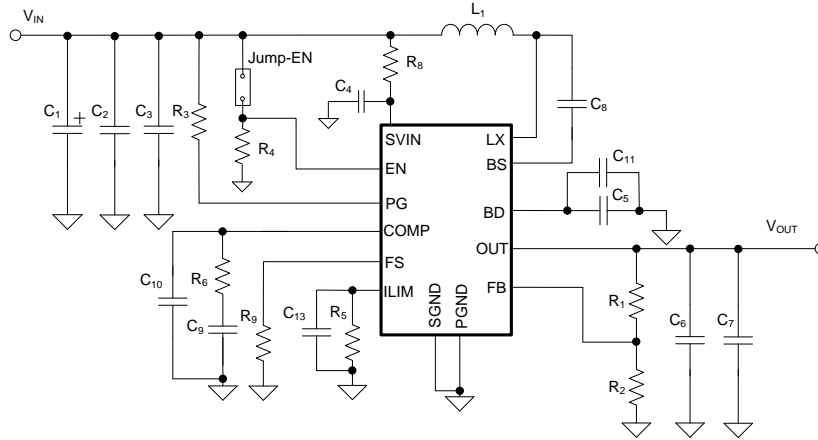
$$C_P = \frac{R_{ESR} \times C_O}{R_Z}$$

### **Soft Start Circuit**

The SY21225 includes a soft-start circuit that is used to limit the in-rush current during the device power up sequence. Using the recommended output capacitors for the BD and OUT pins the typical soft-start time is about 2ms. When larger capacitance and output current are used on the output, the soft-start time will proportionally increase.

## Typical Design

### Typical Schematic



### Design Specifications

Input Voltage (V)	Output Voltage (V)	Output Current Limit (A)
4.5-10	12	3

### BOM List

Reference Designator	Description	Part Number	Manufacturer
C <sub>1</sub>	220μF/35V, Electrolytic Capacitor		
C <sub>3</sub> , C <sub>5</sub> , C <sub>6</sub> , C <sub>7</sub> , C <sub>11</sub>	22μF/25V, 1206	C3216X5R1E226M	
C <sub>4</sub>	2.2μF/25V, 1206	C3216X7R1E225K	
C <sub>8</sub>	100nF/50V, 0603	C1608X7R1H104K	
C <sub>9</sub>	1nF/50V, 0603	C1608C0G1H102J	
C <sub>10</sub>	22pF/50V, 0603	C1608C0G1H220J	
C <sub>13</sub>	10pF/50V, 0603	C1608C0G1H100D	
R <sub>1</sub>	110kΩ, 0603		
R <sub>2</sub>	10kΩ, 0603		
R <sub>3</sub>	100kΩ, 0603		
R <sub>4</sub>	1MΩ, 0603		
R <sub>5</sub>	7.5kΩ, 0603		
R <sub>6</sub>	30kΩ, 0603		
R <sub>8</sub>	10Ω, 0603		
R <sub>9</sub>	390kΩ, 0603		
L <sub>1</sub>	2.2μH/12A	PIMB104T-2R2MS	

### Recommend Table for Typical Applications

V <sub>OUT</sub> (V)	R <sub>H</sub> (kΩ)	R <sub>L</sub> (kΩ)	L(μH)	C <sub>OUT</sub>
12	110	10	2.2	2*22μF/25V/X7R,1206
24	230	10	2.2	2*22μF/25V/X7R,1206

## Layout Design

To achieve a higher efficiency and better noise immunity, following components should be placed close to the IC:  $C_{IN}$ ,  $C_{BD}$ ,  $C_{OUT}$ ,  $L$ ,  $R_1$  and  $R_2$ .

- 1) It is desirable to maximize the PCB copper area connecting to PGND pin to achieve a better thermal performance and noise immunity. A designated ground plane layer is highly recommended.
- 2)  $C_{SVIN}$  must be close to SVIN and SGND pins. The loop area formed by  $C_{SVIN}$ , SVIN and SGND pins must be minimized.
- 3)  $C_{BD}$  must be close to BD and the PGND pins. The loop area formed by  $C_{BD}$ , BD and the PGND pins must be minimized.
- 4) The PCB copper area associated with the LX pin must be minimized to improve the noise immunity.
- 5) The components  $R_1$  and  $R_2$  and the trace connecting to the FB pin must NOT be adjacent to the LX node on the PCB layout to minimize the noise coupling to FB pin.
- 6) If the system chip interfacing with the EN pin has a high impedance state at shutdown mode and the SVIN pin is connected directly to a power source such as a Li-Ion battery, it is desirable to add a pull-down  $1M\Omega$  resistor across the EN and SGND pins to prevent noise from falsely turning on the regulator while in shutdown mode.

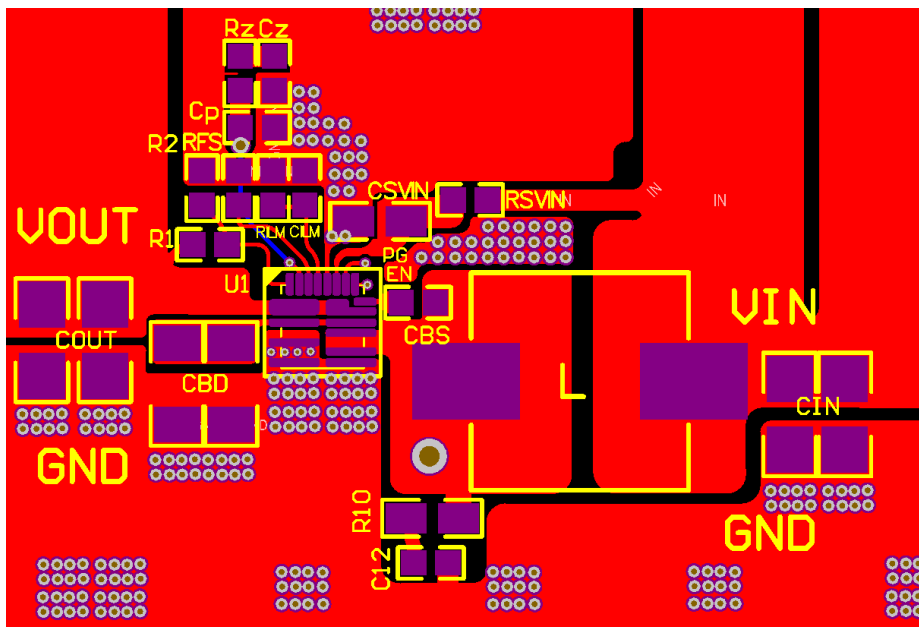
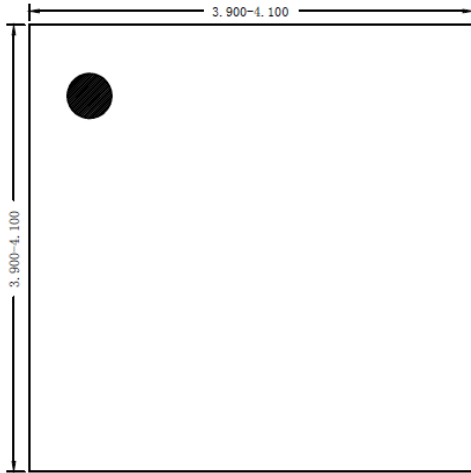
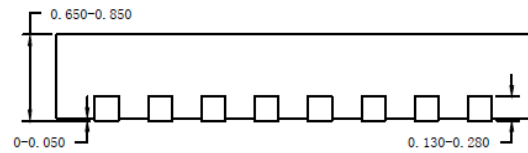


Figure4. PCB Layout Suggestion

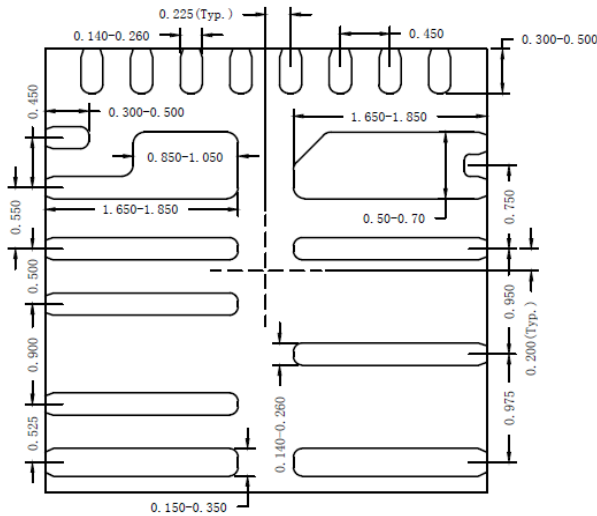
**QFN4x4-18 Package Outline Drawing**



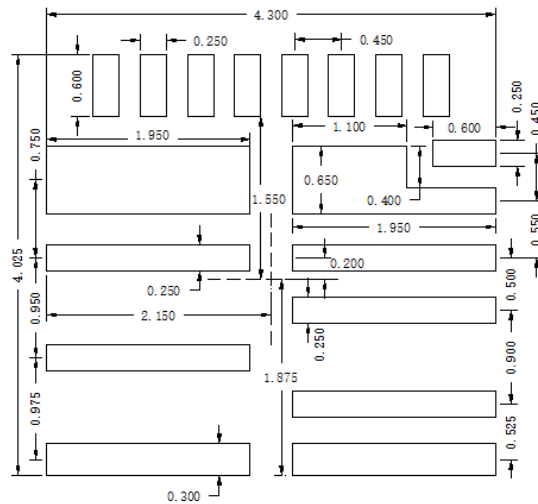
**Top View**



**Side View**



**Bottom View**



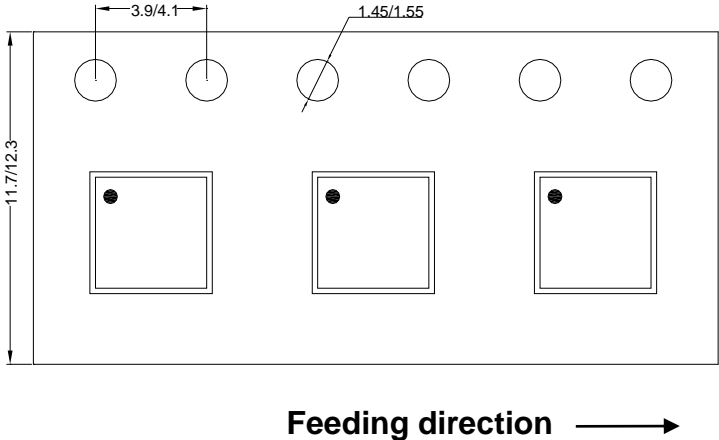
**Recommended PCB layout  
(Reference only)**

**Notes: All dimensions in millimeter and exclude mold flash & metal burr;  
The center of PCB diagram refers to chip body center.**

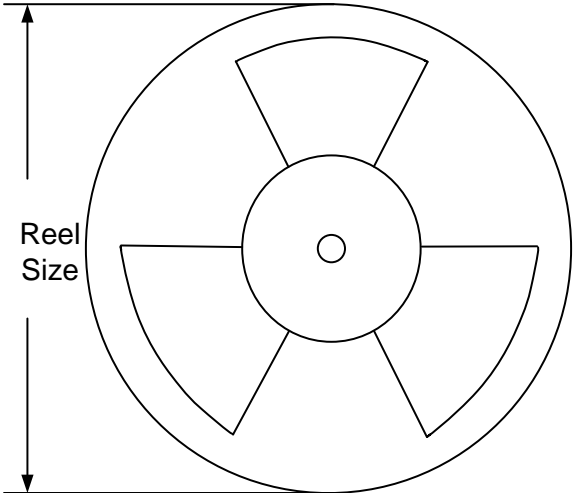
### Taping & Reel Specification

#### 1. Taping orientation

QFN4x4



#### 2. Carrier Tape & Reel specification for packages



Package types	Tape width (mm)	Pocket pitch(mm)	Reel size (Inch)	Trailer length(mm)	Leader length (mm)	Qty per reel
QFN4x4	12	8	13"	400	400	5000

#### 3. Others: NA



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## Revision History

The revision history provided is for informational purpose only and is believed to be accurate, however, not warranted. Please make sure that you have the latest revision.

Date	Revision	Change
Apr.20, 2023	Revision 1.0	Language improvements for clarity.
Nov.05, 2019	Revision 0.9	Initial Release



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