

General Description

The SY20118A high-efficiency 1MHz synchronous step-down DC/DC regulator operates over a wide input voltage range of 2.5V to 5.5V, and can deliver an output current up to 4A with a low quiescent current of 55 μ A. It integrates a main switch and a synchronous switch with very low $R_{DS(ON)}$ to minimize conduction loss. The 1MHz switching frequency allows for low output-voltage ripple, as well as small external inductor and capacitor values.

The SY20118A is highly integrated, so only the input and output capacitors, inductor, and feedback resistors need to be selected for the targeted application specifications.

The SY20118A is available in a compact DFN2x2-8 package.

Features

- 2.5V to 5.5V Input Voltage Range
- Up to 4A Output Current
- Low $R_{DS(ON)}$ for Internal Switches: 85m Ω Top, 60m Ω Bottom
- Low 55 μ A Quiescent Current
- High 1MHz Switching Frequency Minimizes Required External Components
- Internal Soft-Start Limits the Inrush Current
- 100% Dropout Operation
- Power-Good Indicator
- Hiccup Mode for Short-Circuit Protection
- Output Auto-Discharge Function
- RoHS-Compliant and Halogen-Free
- Compact Package: DFN2x2-8

Applications

- Set-Top Box
- USB Dongle
- Media Player
- Smartphone

Typical Application

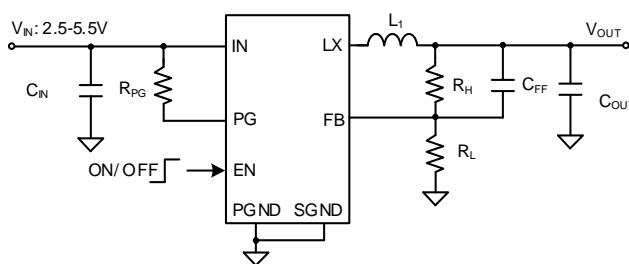


Figure 1. Typical Application Circuit

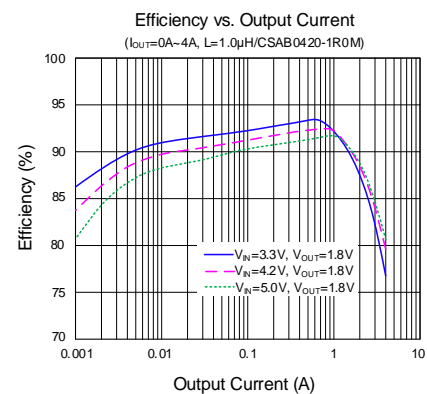


Figure 2. Efficiency vs. Output Current

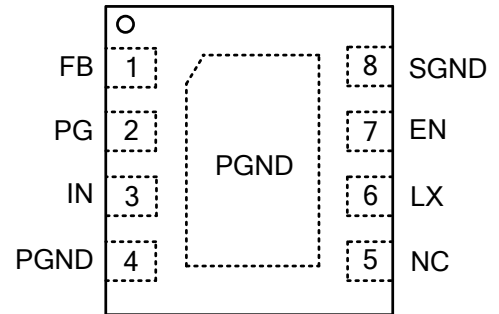


Ordering Information

Ordering Part Number	Package type	Top Mark
SY20118ADFC	DFN2x2-8 RoHS Compliant and Halogen Free	t2xyz

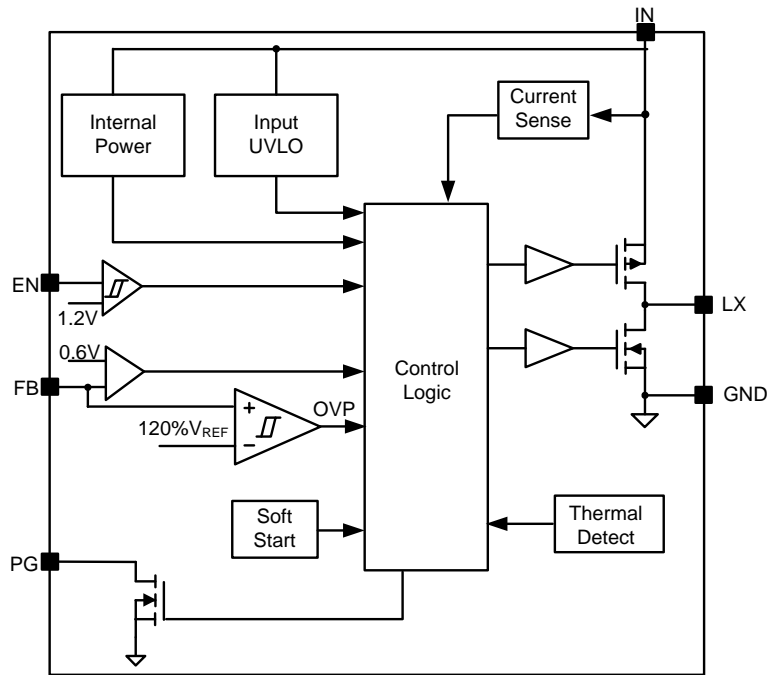
x = year code, y = week code, z = lot number code

Pinout (top view)



Pin Description

Pin No	Pin Name	Pin Description
1	FB	Output feedback pin. Connect this pin to the center point of the output resistor-divider. See application information.
2	PG	Power-good indicator. Open-drain output. Hi-Z (high impedance) when the output voltage is within 90% to 120% of the regulation setpoint. Driven low when voltage outside of this range.
3	IN	Power input. Decouple this pin from the GND pin with at least a 10 μ F ceramic capacitor.
4/EP	PGND	Power ground. Pin 4 and exposed pad.
5	NC	No connection.
6	LX	Inductor pin. Connect this pin to the switching node of the inductor.
7	EN	Enable pin. Pull low to disable the device, pull high to enable. Do not leave this pin floating.
8	SGND	Analog ground.

Block Diagram

Figure 3. Block Diagram
Absolute Maximum Ratings

Parameter (Note 1)	Min	Max	Unit
IN	-0.3	6	V
EN, FB, PG	-0.3	IN + 0.6	
LX	-0.3	6	
LX, 20ns duration	-3	7	
Junction Temperature, Operating	-40	150	°C
Lead Temperature (Soldering, 10s)		260	
Storage Temperature	-65	150	

Thermal Information

Parameter (Note 2)	Type	Unit
θ_{JA} Junction-to-Ambient Thermal Resistance	70	°C/W
θ_{JC} Junction-to-Case Thermal Resistance	25	
P_D Power Dissipation $T_A = 25^\circ\text{C}$	1.4	W

Recommended Operating Conditions

Parameter (Note 3)	Min	Max	Unit
IN	2.5	5.5	V
Output Voltage	0.6	5.5	
Output Current		4	A
Junction Temperature	-40	125	°C

Electrical Characteristics

($V_{IN} = 5V$, $V_{OUT} = 1.8V$, $L = 1.0\mu H$, $C_{OUT} = 32\mu F$, $T_J = 25^\circ C$, unless otherwise specified)

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit	
Input	Voltage	V_{IN}		2.5		5.5	V	
	UVLO, rising	$V_{IN,UVLO}$			2.45	2.5	V	
	UVLO, hysteresis	$V_{IN,HYS}$			150		mV	
	Quiescent current	I_Q	$V_{FB} = 105\% \times V_{REF}$		55		μA	
	Shutdown current	I_{SHDN}	$V_{EN} = 0V$		0.1	1	μA	
FB	Reference voltage	V_{REF}	$I_{OUT} = 0.5A$, CCM	0.591	0.6	0.609	V	
	Input current	I_{FB}	$V_{EN} = 2V$, $V_{FB} = 1V$	-50	0	50	nA	
Power Switch	On resistance	$R_{DS(ON)HS}$			85		m Ω	
	Current limit	$I_{LMT,HS}$		4.7			A	
Synchronous Rectifier	On resistance	$R_{DS(ON)LS}$			60		m Ω	
Discharge FET resistance		R_{DIS}			50		Ω	
Enable(EN)	Input voltage high	$V_{EN,H}$		1.2			V	
	Input voltage low	$V_{EN,L}$				0.4	V	
	Input current	I_{EN}	$V_{EN} = 2V$			2	μA	
Soft-Start (SS)	Turn-on delay time	$t_{ON,DLY}$	From EN high to LX start switching		0.5		ms	
	Soft-start time	t_{SS}	V_{OUT} from 0% to 100%		1		ms	
Undervoltage Protection	Threshold	V_{UVP}			50		% V_{REF}	
	Delay	$t_{UVP,DLY}$			10		μs	
UVP/OCP Hiccup ON Time		$t_{HICCUP,ON}$			3.5		ms	
UVP/OCP Hiccup OFF Time		$t_{HICCUP,OFF}$			3.5		ms	
Power Good	Thresholds	V_{PG}	V_{FB} falling, fault		88		%	
			V_{FB} rising, good		90		%	
			V_{FB} rising, fault		120		%	
			V_{FB} falling, good		114		%	
	Delay		$t_{PG,R}$	V_{FB} rising, good		2		μs
			$t_{PG,F}$	V_{FB} falling, fault		20		μs
Switching Frequency		f_{SW}	$I_{OUT} = 0.5A$, CCM		1		MHz	
Min ON Time		$t_{ON,MIN}$			50		ns	
Maximum Duty Cycle		D_{MAX}		100			%	
Thermal Shutdown Temperature		T_{SD}			160		$^\circ C$	
Thermal Shutdown Hysteresis		T_{HYS}			20		$^\circ C$	

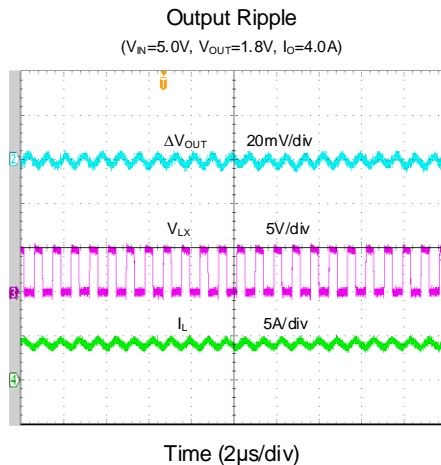
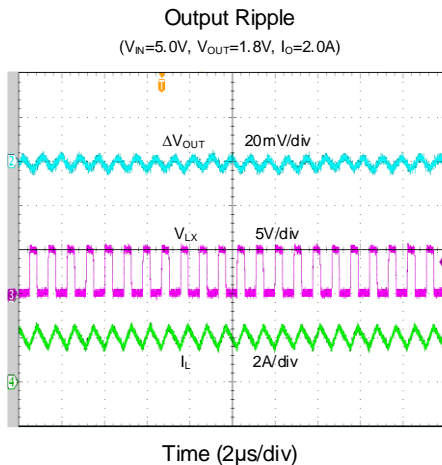
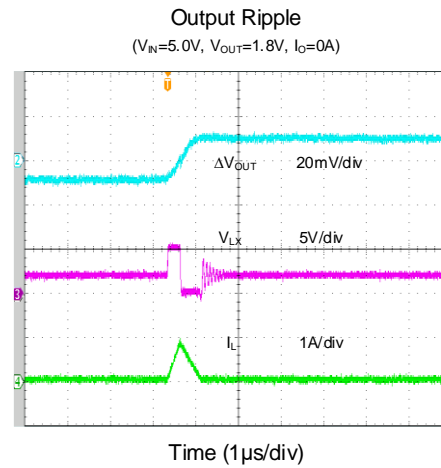
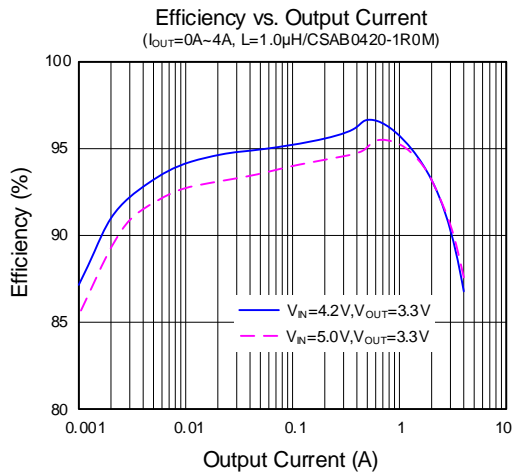
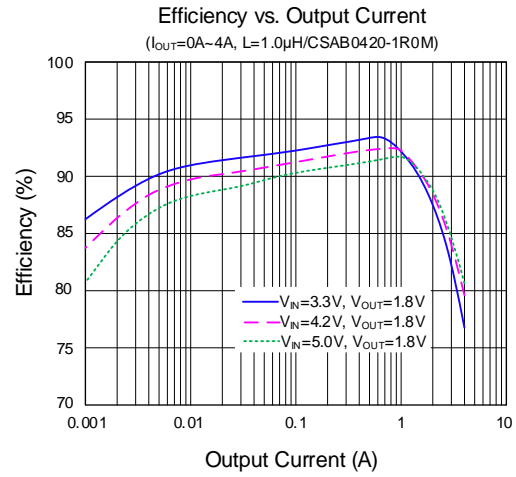
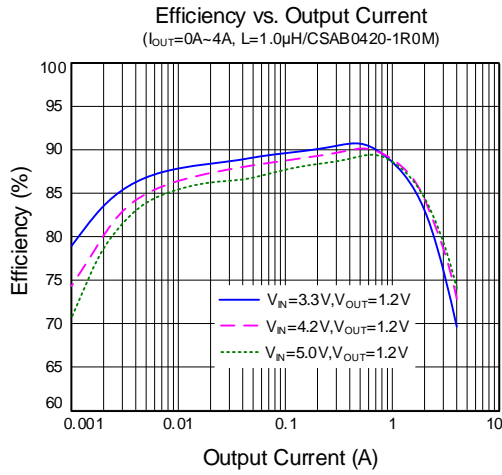
Note 1: Stresses beyond the "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Note 2: θ_{JA} of SY20118ADFC is measured in the natural convection at $T_A = 25^\circ C$ on a 2oz two-layer Silergy evaluation board. Paddle of DFN2x2-8 package is the case position for θ_{JC} measurement.

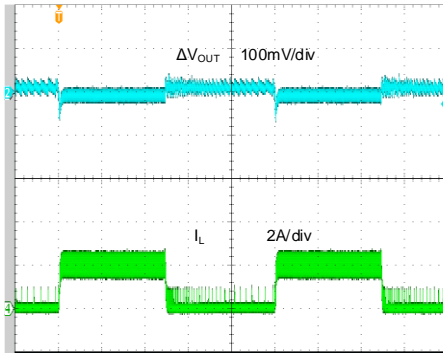
Note 3: The device is not guaranteed to function outside its operating conditions.

Typical Performance Characteristics

($T_A = 25^\circ\text{C}$, $V_{IN} = 5\text{V}$, $V_{OUT} = 1.8\text{V}$, $L = 1.0\mu\text{H}$, $C_{OUT} = 32\mu\text{F}$, unless otherwise noted)

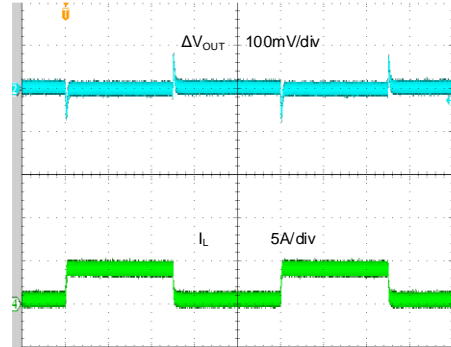


Load Transient
($V_{IN}=5.0V$, $V_{OUT}=1.8V$, $I_O=0A \sim 2.0A$)



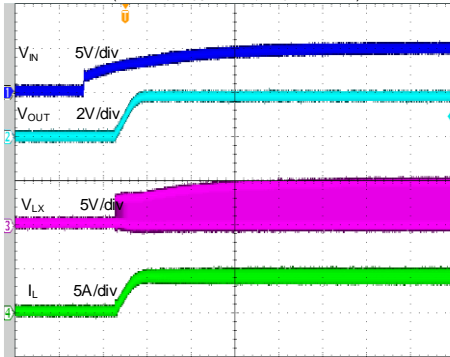
Time (200μs/div)

Load Transient
($V_{IN}=5.0V$, $V_{OUT}=1.8V$, $I_O=0.4A \sim 4.0A$)



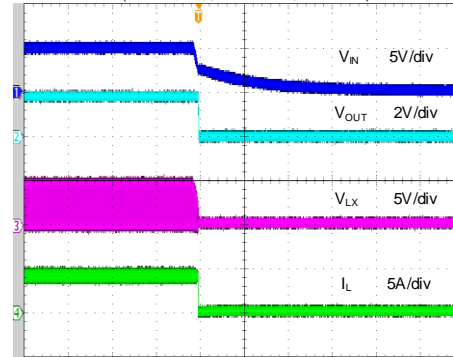
Time (200μs/div)

Startup from V_{IN}
($V_{IN}=5V$, $V_{OUT}=1.8V$, $R_{LOAD}=0.45\Omega$)



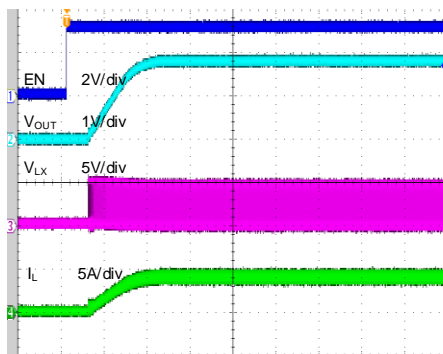
Time (2ms/div)

Shutdown from V_{IN}
($V_{IN}=5V$, $V_{OUT}=1.8V$, $R_{LOAD}=0.45\Omega$)



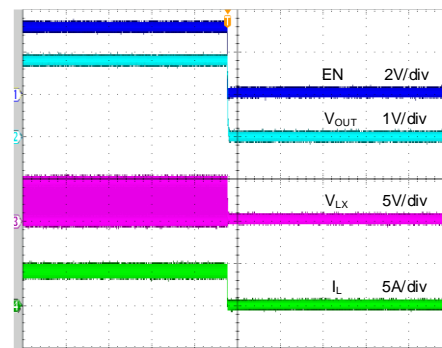
Time (2ms/div)

Startup from Enable
($V_{IN}=5.0V$, $V_{OUT}=1.8V$, $R_{LOAD}=0.45\Omega$)



Time (800μs/div)

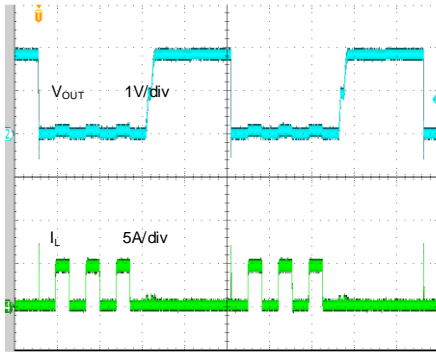
Shutdown from Enable
($V_{IN}=5.0V$, $V_{OUT}=1.8V$, $R_{LOAD}=0.45\Omega$)



Time (800μs/div)

Short Circuit Protection

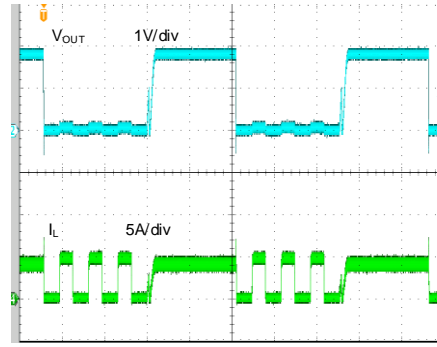
($V_{IN}=5.0V$, $V_{OUT}=1.8V$, $I_O=0A$ - Short)



Time (10ms/div)

Short Circuit Protection

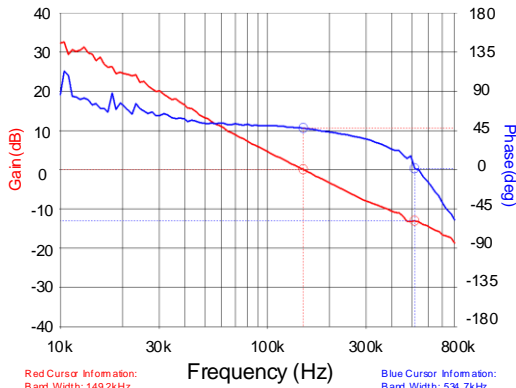
($V_{IN}=5.0V$, $V_{OUT}=1.8V$, $I_O=4.0A$ - Short)



Time (10ms/div)

Bode Plot

($V_{IN}=5V$, $V_{OUT}=1.8V$, $I_{OUT}=4A$)

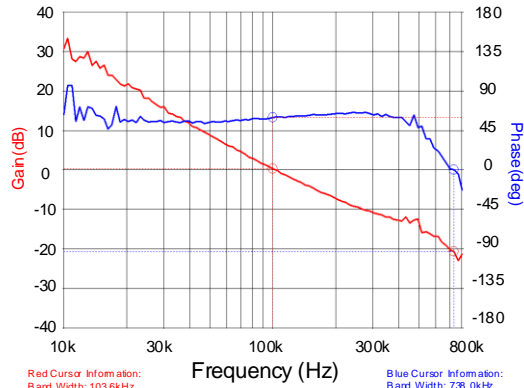


Red Cursor Information:
Band Width: 149.2kHz
Phase Margin: 47.4 deg

Blue Cursor Information:
Band Width: 534.7kHz
Gain: -13.3dB

Bode Plot

($V_{IN}=5V$, $V_{OUT}=3.3V$, $I_{OUT}=4A$)



Red Cursor Information:
Band Width: 103.6kHz
Phase Margin: 60.0 deg

Blue Cursor Information:
Band Width: 738.0kHz
Gain: -20.8dB

Operation

The SY20118A high-efficiency 1MHz synchronous step-down DC/DC regulator operates over a wide input voltage range of 2.5V to 5.5V, and can deliver an output current up to 4A with a low quiescent current of 55µA. To minimize conduction loss, it integrates a main switch and a synchronous switch with very low $R_{DS(ON)}$. The 1MHz switching frequency allows for low output-voltage ripple, as well as small external inductor and capacitor values.

The SY20118A employs a constant-off-time and peak-current-mode control strategy. When the top FET's current-sense signal reaches internal V_{COMP} , the top FET turns off and the bottom FET turns on for a fixed period of time (constant t_{OFF}). t_{OFF} is internally calculated according to the input voltage, output voltage, and desired switching frequency (f_{SW}):

$$t_{OFF} = \frac{1 - V_{OUT}/V_{IN}}{f_{SW}}$$

The bottom FET turns off after a period of t_{OFF} .

The SY20118A is available in a compact DFN2x2-8 package.

Application Information

The SY20118A is highly integrated, so only the input capacitor C_{IN} , the output capacitor C_{OUT} , the output inductor L , and the feedback resistors R_H and R_L need to be selected for the targeted application specifications.

Feedback Resistor-Divider R_H and R_L

Choose R_H and R_L to program the proper output voltage. A value between 1kΩ and 1MΩ is recommended for both resistors. If R_L is chosen as 120kΩ, for example, then R_H can be calculated as follows:

$$R_H = \frac{(V_{OUT} - 0.6V) \times R_L}{0.6V}$$

Input Capacitor C_{IN}

For the best performance, select a typical X5R or better grade ceramic capacitor with a 10V rating, and greater than 10µF capacitance. The capacitor should be placed as close as possible to the device, while also minimizing the loop area formed by C_{IN} and the IN/GND pins.

When selecting an input capacitor, ensure that its voltage rating is at least 20% greater than the maximum voltage of the input supply. X5R or X7R dielectric types are the most often selected due to their small size, low cost, surge current capability, and high RMS current rating over a wide temperature and voltage range.

In situations where the input rail is supplied through long wires, it is recommended to add some bulk capacitance like electrolytic, tantalum or polymer type capacitors to reduce the overshoot and ringing caused by the added parasitic inductance.

Consider the RMS current rating of the input capacitor, paralleling additional capacitors if required to meet the calculated RMS ripple current.

$$I_{CIN_RMS} = I_{OUT} \times \sqrt{D \times (1 - D)}$$

The worst-case condition occurs at $D = 0.5$, then

$$I_{CIN_RMS_MAX} = \frac{I_{OUT}}{2}$$

For simplicity, use an input capacitor with an RMS current rating greater than 50% of the maximum load current.

The input capacitor value determines the input voltage ripple of the converter. If there is a voltage ripple requirement in the system, choose an appropriate input capacitor that meets the specification.

Given the very low ESR and ESL of ceramic capacitors, the input voltage ripple can be estimated using the formula:

$$V_{CIN_RIPPLE_CAP} = \frac{I_{OUT}}{f_{SW} \times C_{IN}} \times D \times (1 - D)$$

The worst-case condition occurs at $D = 0.5$, then

$$V_{CIN_RIPPLE_CAP_MAX} = \frac{I_{OUT}}{4 \times f_{SW} \times C_{IN}}$$

The capacitance value is less important than the RMS current rating. A single 10µF X5R capacitor is sufficient in most applications.

Output Capacitor C_{OUT}

Select the output capacitor C_{OUT} to handle the output ripple requirements. Both steady-state ripple and transient requirements must be taken into consideration when selecting C_{OUT}. For the best performance, use an X5R or better grade ceramic capacitor with a 6.3V rating, and capacitance greater than 32μF.

For applications where the design must meet stringent ripple requirements, the following considerations must be followed.

The output voltage ripple at the switching frequency is caused by the inductor-current ripple (ΔI_L) on the output capacitor's ESR (ESR ripple), as well as the stored charge (capacitive ripple). When calculating total ripple, consider both.

$$V_{RIPPLE,ESR} = \Delta I_L \times ESR$$

$$V_{RIPPLE,CAP} = \frac{\Delta I_L}{8 \times C_{OUT} \times f_{SW}}$$

The capacitive ripple might be higher because the effective capacitance for ceramic capacitors decreases with the voltage across the terminals. The voltage derating is usually included as a chart in the capacitor datasheet, and the ripple can be recalculated after taking the target output voltage into account.

Output Inductor L

Consider the following when choosing this inductor:

- 1) Choose the inductance to provide a ripple current that is approximately 40% of the maximum output current. The recommended inductance is calculated as:

$$L = \frac{V_{OUT}(1 - V_{OUT} / V_{IN,MAX})}{f_{SW} \times I_{OUT,MAX} \times 0.4}$$

where f_{SW} is the switching frequency and I_{OUT,MAX} is the maximum load current.

The SY20118A has high tolerance for ripple current amplitude variation. As a result, the final choice of inductance can vary slightly from the calculated value with no significant performance impact.

- 2) The inductor's saturation current rating must be greater than the peak inductor current under full load:

$$I_{SAT,MIN} > I_{OUT,MAX} + \frac{V_{OUT}(1 - V_{OUT}/V_{IN,MAX})}{2 \times f_{SW} \times L}$$

- 3) The DCR of the inductor and the core loss at the switching frequency must be low enough to achieve the desired efficiency requirement. Use an inductor with DCR less than 30mΩ to achieve good overall efficiency.

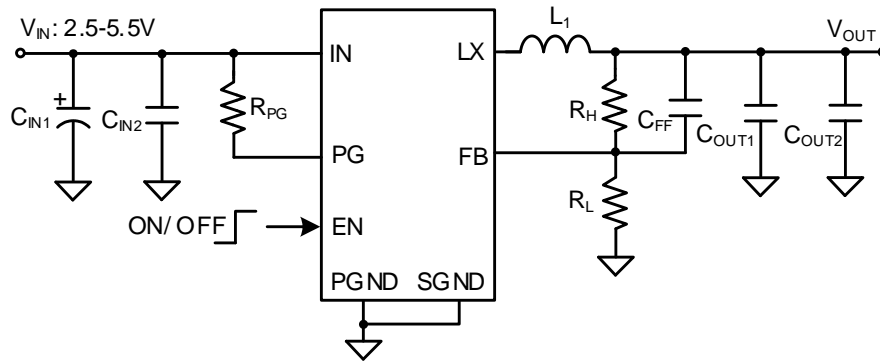
Overcurrent and Short-Circuit Protection

With load current increasing, as soon as the high-side FET current exceeds the peak current-limit threshold, the high-side FET will turn off. If the load current continues to increase, the output voltage will drop. When the output voltage falls below 50% of the regulation level, the output undervoltage protection will be activated and the SY20118A will operate in hiccup mode. The hiccup frequency is 400Hz and the hiccup duty cycle is 50%. If the hard short is removed, the SY20118A will return to normal operation.

Load-Transient Considerations

The SY20118A integrates compensation components to achieve fast transient responses and improved stability. In some applications, adding a ceramic capacitor (feed-forward capacitor C_#) in parallel with R_H may further speed up the load-transient responses, and is therefore recommended for applications with large load-transient step requirements.

Application Schematic ($V_{OUT} = 1.8V$)



BOM List

Reference Designator	Description	Part Number	Manufacturer
L1	1.0 μ H Inductor	CSAB0420-1R0M	CODACA
C _{IN1}	100 μ F/25V(electrolytic capacitor)		
C _{IN2}	10 μ F/10V, 0805, X5R	C2012X5R1A106K	TDK
C _{OUT1}	22 μ F/6.3V, 0805, X5R	C2012X5R0J226M	TDK
C _{OUT2}	10 μ F/10V, 0805, X5R	C2012X5R1A106K	TDK
C _{ff}	10pF/50V, 0603, C0G	C1608C0G1H100D	TDK
R _H	100k Ω , 1%, 0603		
R _L	49.9k Ω , 1%, 0603		
R _{PG}	100k Ω , 0603		

Recommend Components for Typical Applications

V _{OUT} (V)	R _H (k Ω)	R _L (k Ω)	C _{FF} (pF)	L/(Rated/Saturating Current)	C _{OUT1}	C _{OUT2}
1.2	49.9	49.9	22	1.0 μ H/(6.2A/9A)	22 μ F/6.3V, 0805, X5R	22 μ F/6.3V, 0805, X5R
1.8	100	49.9	10	1.0 μ H/(6.2A/9A)	22 μ F/6.3V, 0805, X5R	10 μ F/10V, 0805, X5R
3.3	100	22.1	10	1.0 μ H/(6.2A/9A)	22 μ F/6.3V, 0805, X5R	10 μ F/10V, 0805, X5R

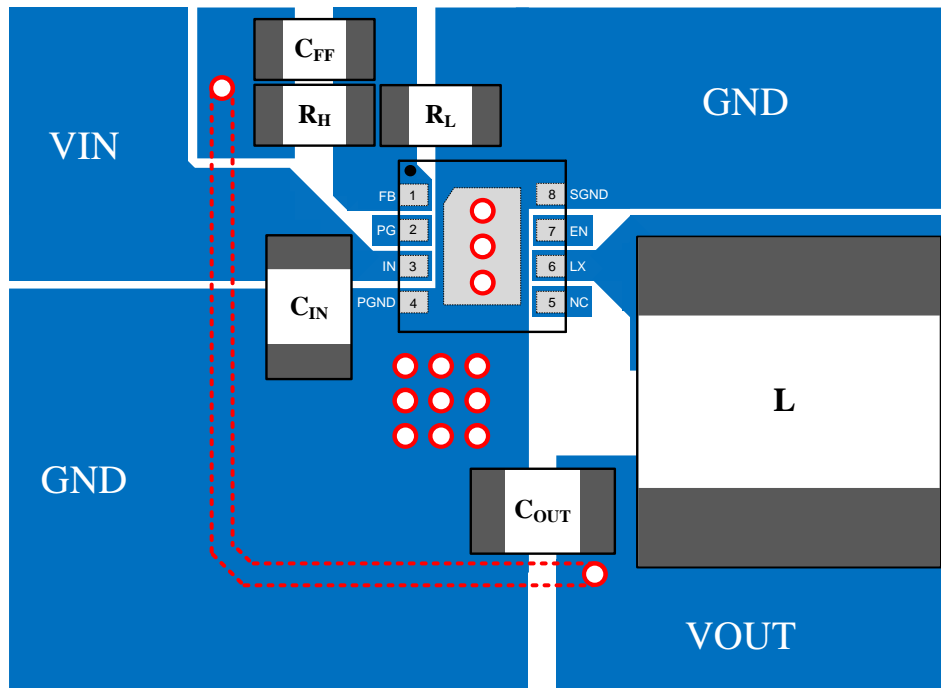


Layout Design

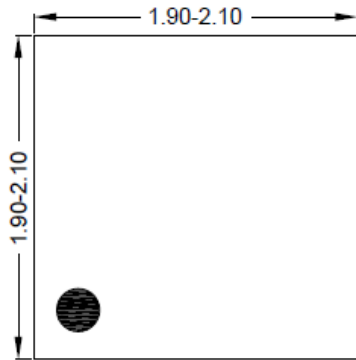
For optimal design, follow these PCB layout considerations:

- For minimum noise and maximum efficiency, place the following components close to the IC: C_{IN} , L, R_H and R_L .
- To achieve the best thermal and noise performance, maximize the PCB copper area connecting to the GND pin. A ground plane is highly recommended if board space allows.

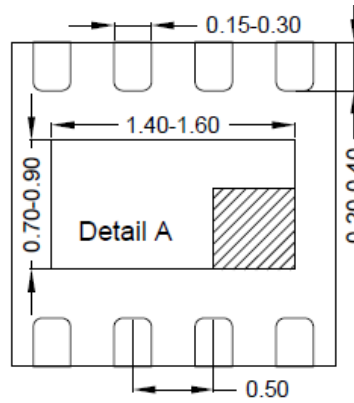
- C_{IN} must be close to pins IN and GND. Minimize the loop area formed by C_{IN} , V_{IN} , and GND.
- To reduce potential noise:
 - Minimize the PCB copper area connected to the LX pin.
 - R_1 , R_2 , and the trace connected to the FB pin must **not** be adjacent to the LX net on the PCB layout.



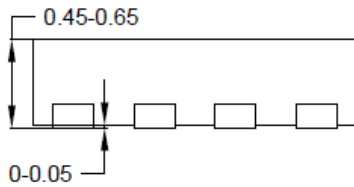
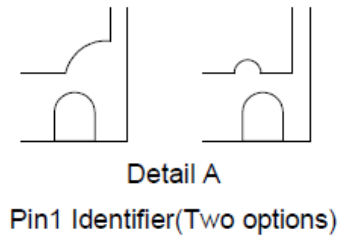
DFN2x2-8 Package Outline Drawing



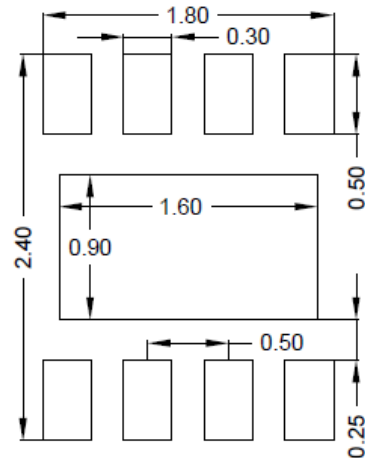
Top view



Bottom view



Side view

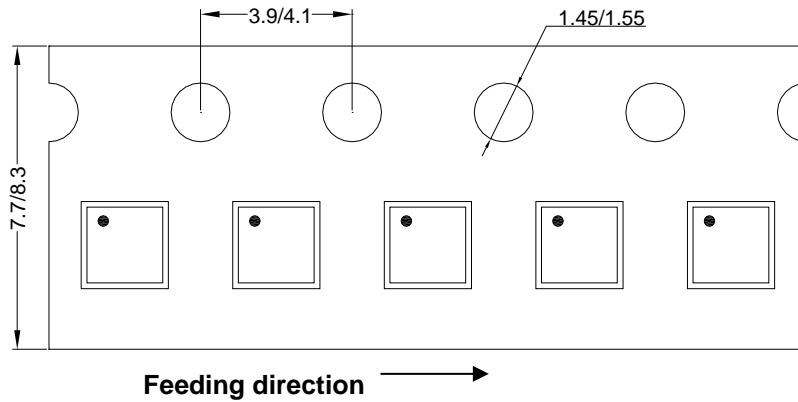


**Recommended PCB layout
(reference only)**

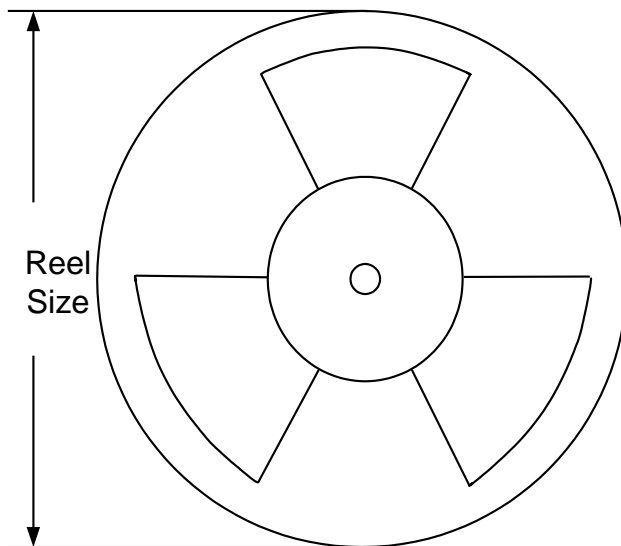
Note: All dimensions are in millimeters and exclude mold flash and metal burr.

Taping and Reel Specification

DFN2x2 taping orientation



Carrier tape and reel specification for packages



Package types	Tape width (mm)	Pocket pitch(mm)	Reel size (Inch)	Trailer length(mm)	Leader length (mm)	Qty per reel
DFN2x2	8	4	7"	400	160	3000

Others: NA

Revision History

The revision history provided is for informational purposes only and is believed to be accurate, however, not warranted. Please make sure that you have the latest revision.

Date	Revision	Change
Nov.10, 2022	Revision 1.0	Product Release
Nov.10, 2021	Revision 0.9	Initial Release

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